



Radio over Multimode Fibre Networks

Ton Koonen, María García Larrodé, Hejie Yang

**COBRA Institute
dept. Electrical Engineering
Eindhoven University of Technology**

e-mail: a.m.j.koonen@tue.nl

***Workshop on Optical/Wireless Integration
OFC'08, San Diego, Feb. 25, 2008***

Outline



- **In-home network architecture for integrated broadband services**
- **Radio-over-MMF using the Optical Frequency Multiplying technique**
- **OFM system experiments**
- **Reconfigurable Radio-over-MMF networks**
- **Concluding remarks**

Versatile BB in-home networks



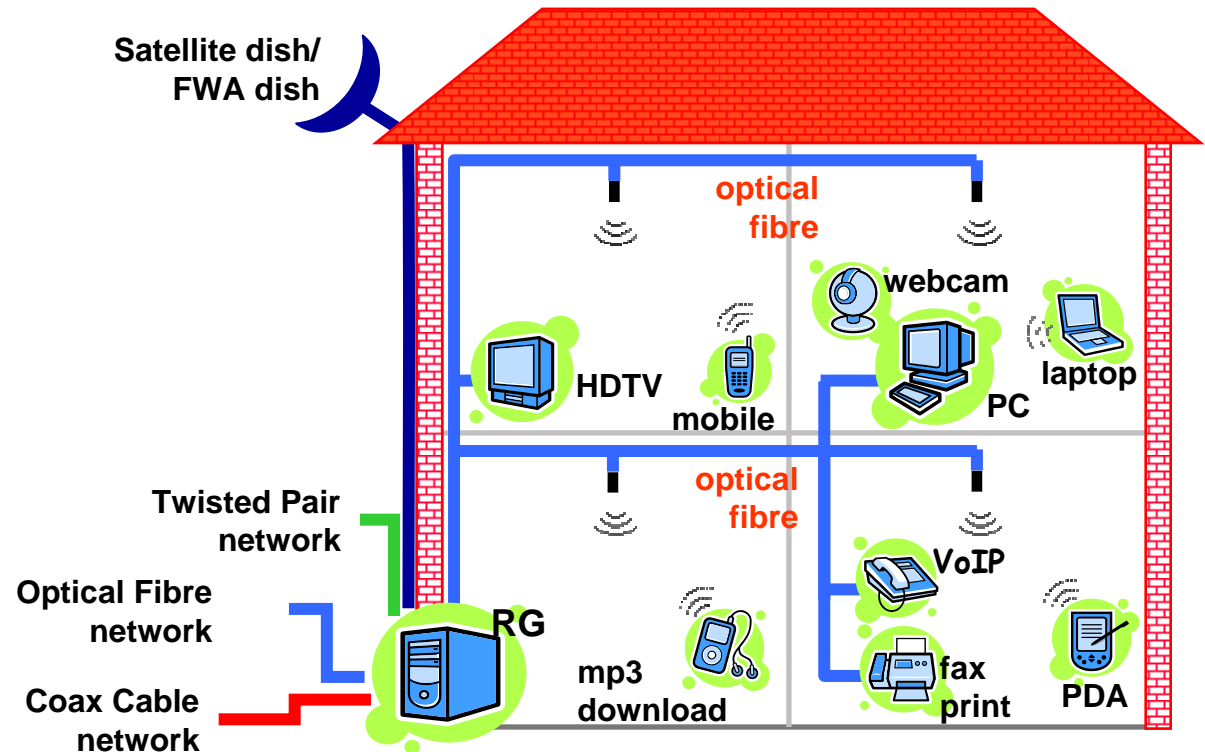
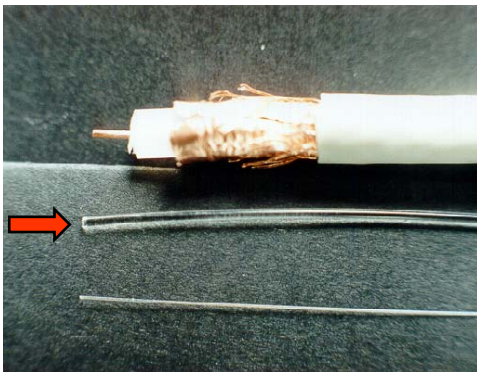
Converged in-home backbone network, integrating wired & wireless services

- reduces installation and maintenance efforts
- eases introduction and upgrading of services

coax

POF

SMF



→ converged in-home network on POF

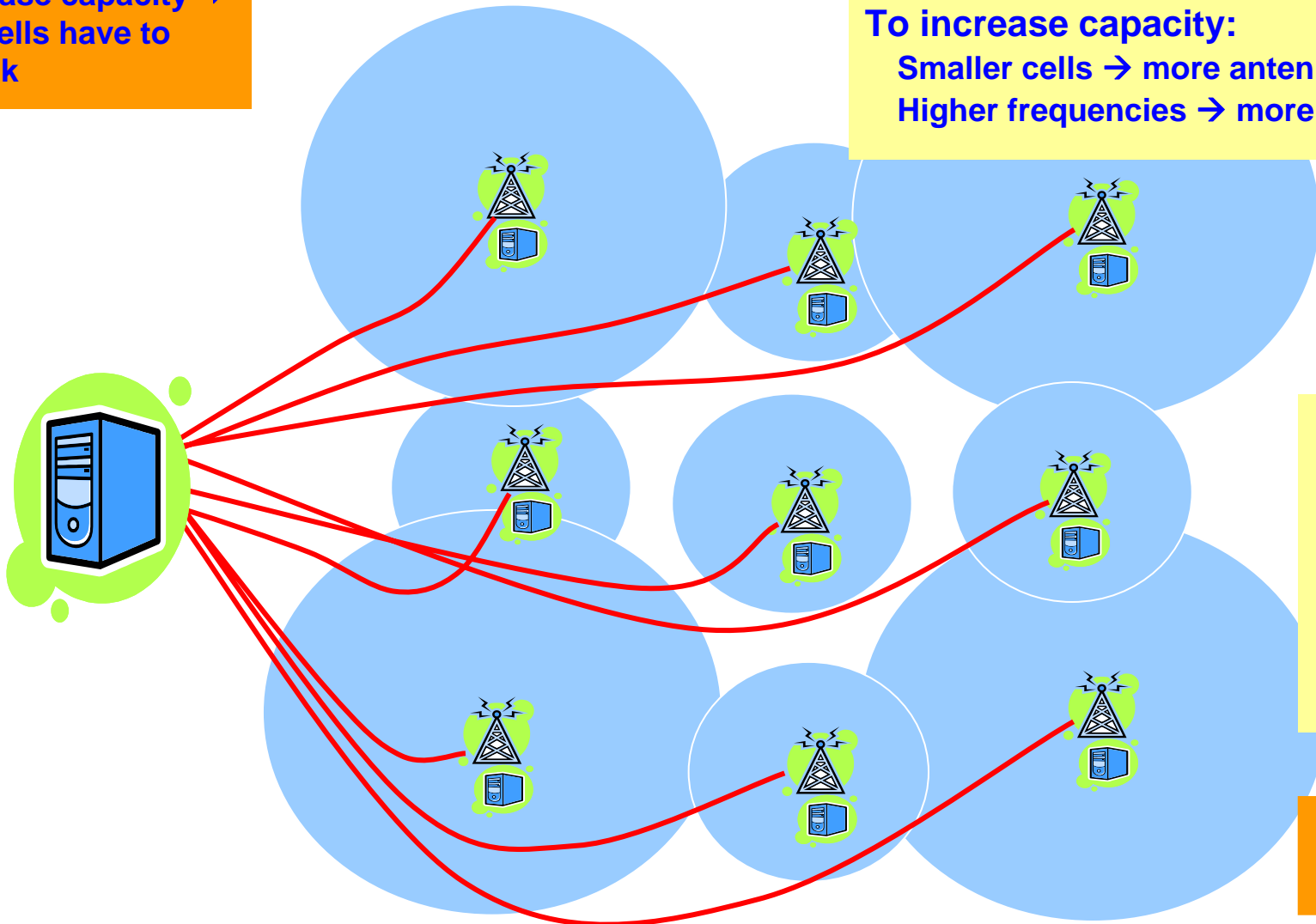
Radio over Fibre

increase capacity \Rightarrow
big cells have to
shrink

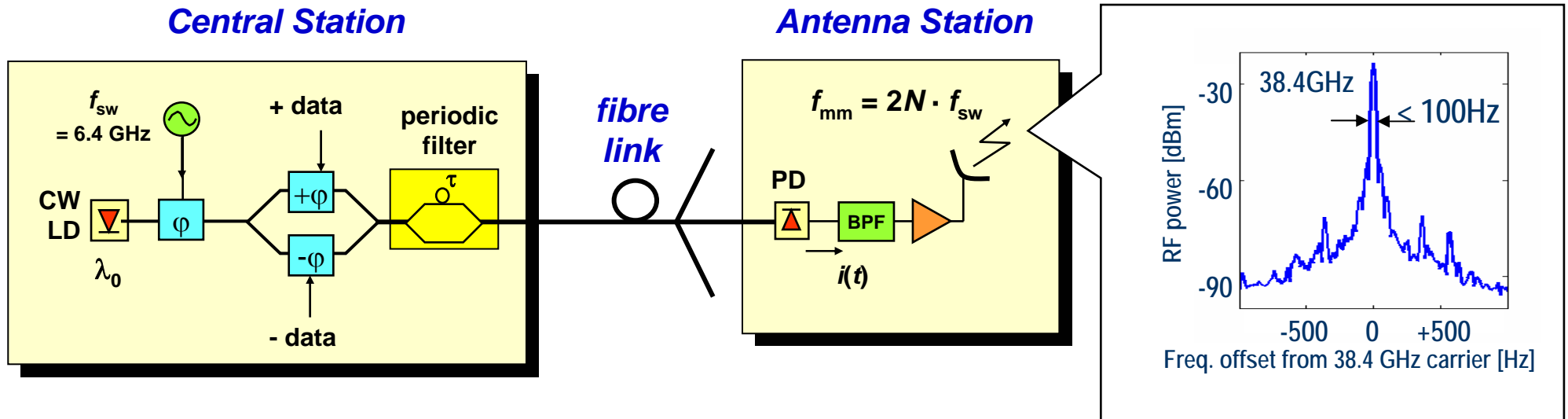
To increase capacity:
Smaller cells \rightarrow more antenna sites
Higher frequencies \rightarrow more complexity

Optical Fibre
Unlimited
bandwidth
Low loss
Light weight
EM immunity

**Radio over
Fibre**



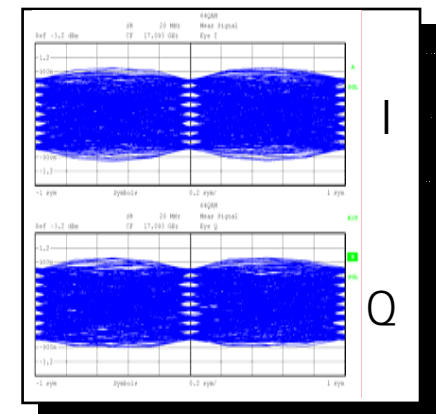
Radio over multimode fibre



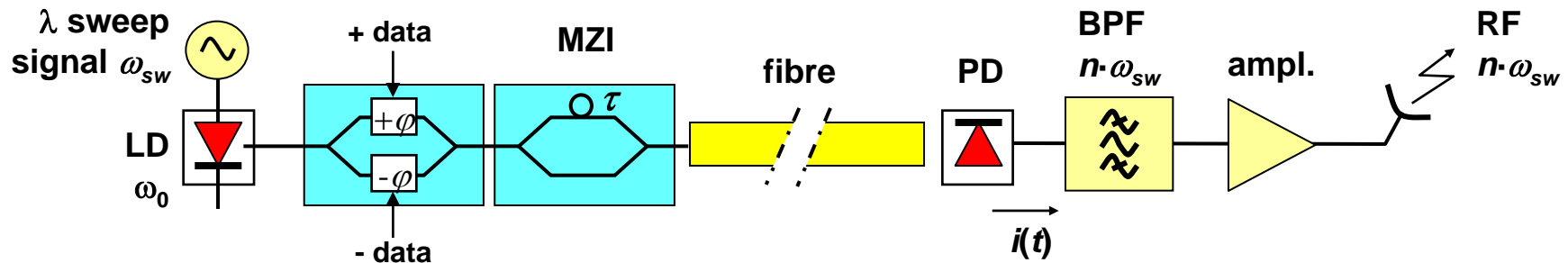
“Optical Frequency Multiplying”

- low-cost technology
- simple antenna stations
- very pure microwave → high wireless capacity
- dispersion-tolerant → for SMF and MMF

120 Mbit/s
64 QAM
@ 17.2 GHz
after 4.4 km
silica MMF



OFM system analysis



- Monochromatic laser, optical frequency ω_0 sinusoidally swept over range $2\beta \cdot \omega_{sw}$ with sweep freq. ω_{sw}
- Periodic bandpass filtering before the fibre (is equivalent to filtering after the fibre)
- MZI with Free Spectral Range $\Delta\Omega_{FSR} = 2\pi / \tau$, locked to laser freq. ω_0
- Neglecting fibre dispersion, photodiode output signal

$$i(t) = I_0 \cdot \left\{ 1 + \cos \left[2\beta \cdot \sin \left(\frac{1}{2} \omega_{sw} \tau \right) \cdot \cos \left(\omega_{sw} \left(t - \frac{1}{2} \tau \right) \right) + \omega_0 \tau \right] \right\}$$

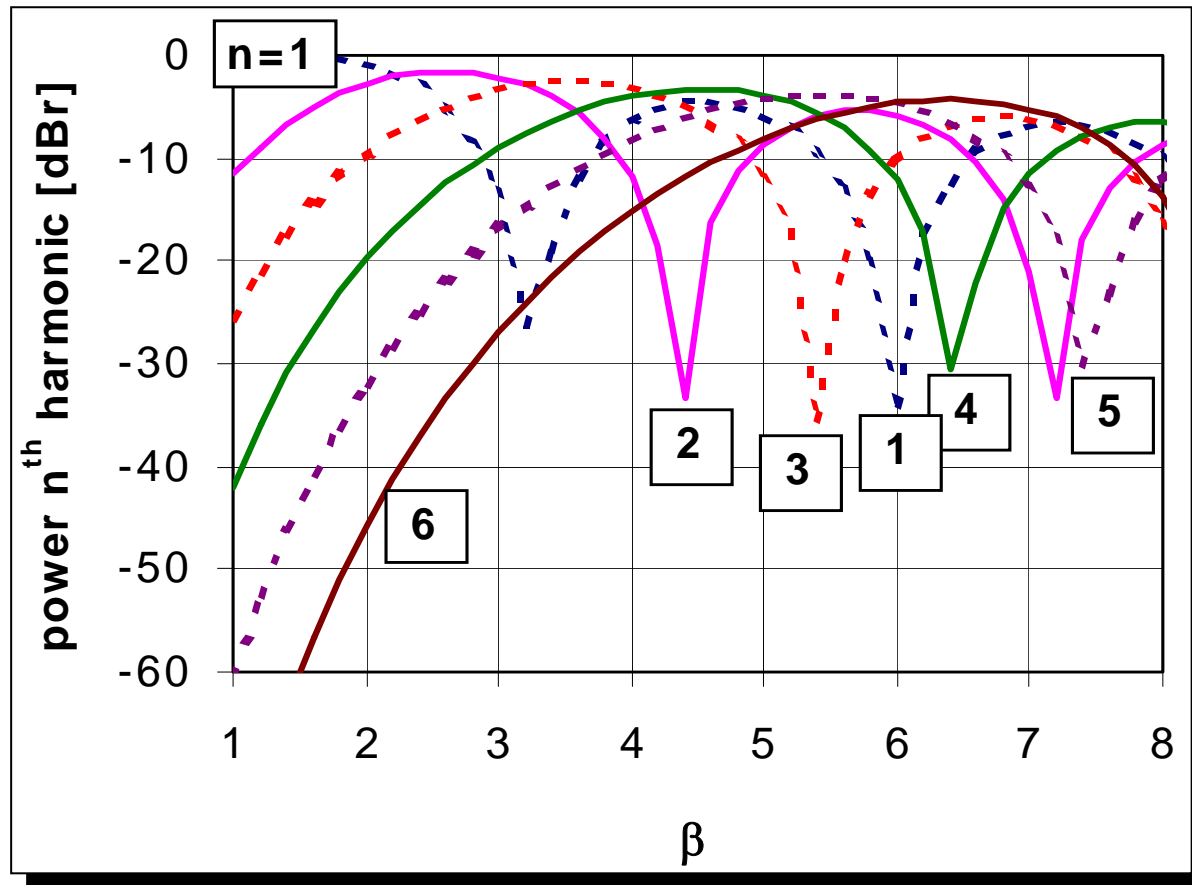
containing even harmonic frequency components at $2k \cdot \omega_{sw}$ with relative amplitude

$$\cos(\omega_0 \tau) \cdot J_{2k} \left(2\beta \cdot \sin \left(\frac{1}{2} \omega_{sw} \tau \right) \right)$$

and odd harmonic frequency components at $(2k+1) \cdot \omega_{sw}$ with relative amplitude

$$\sin(\omega_0 \tau) \cdot J_{2k-1} \left(2\beta \cdot \sin \left(\frac{1}{2} \omega_{sw} \tau \right) \right)$$

OFM generated microwave harmonics



- Assumptions:
 - sweep freq. $f_{SW} = 2$ GHz
 - MZI FSR $\Delta\nu_{FSR} = 10$ GHz
 - at each harmonic, $\omega_0 \tau$ is optimised for max. power

- Optical FM modulation index β to be optimised for max. power in preferred harmonic (e.g., $\beta_{opt} \approx 6.3$ for $n=6$, so for the 12 GHz harmonic)

Impact of laser linewidth



- Output signal of photodiode, assuming laser linewidth $\sqrt{(\delta\omega)^2}$, and neglecting fibre dispersion

$$i(t) = I_0 \cdot \left\{ 1 + \cos\left[2\beta \cdot \sin\left(\frac{1}{2} \omega_{sw} \tau\right) \cdot \cos\left(\omega_{sw} \left(t - \frac{1}{2} \tau\right)\right) + \omega_0 \tau + \delta\omega \cdot \tau\right] \right\}$$

→ OFM effectively suppresses laser phase noise, provided that $\delta\omega_{rms} \cdot \tau \ll \pi / 2$ i.e. laser linewidth is much smaller than a quarter of the FSR of the MZI $\Delta\omega_{FSR} = \pi / 2 \tau$

→ OFM generates very pure microwave carriers

Impact of MMF modal dispersion

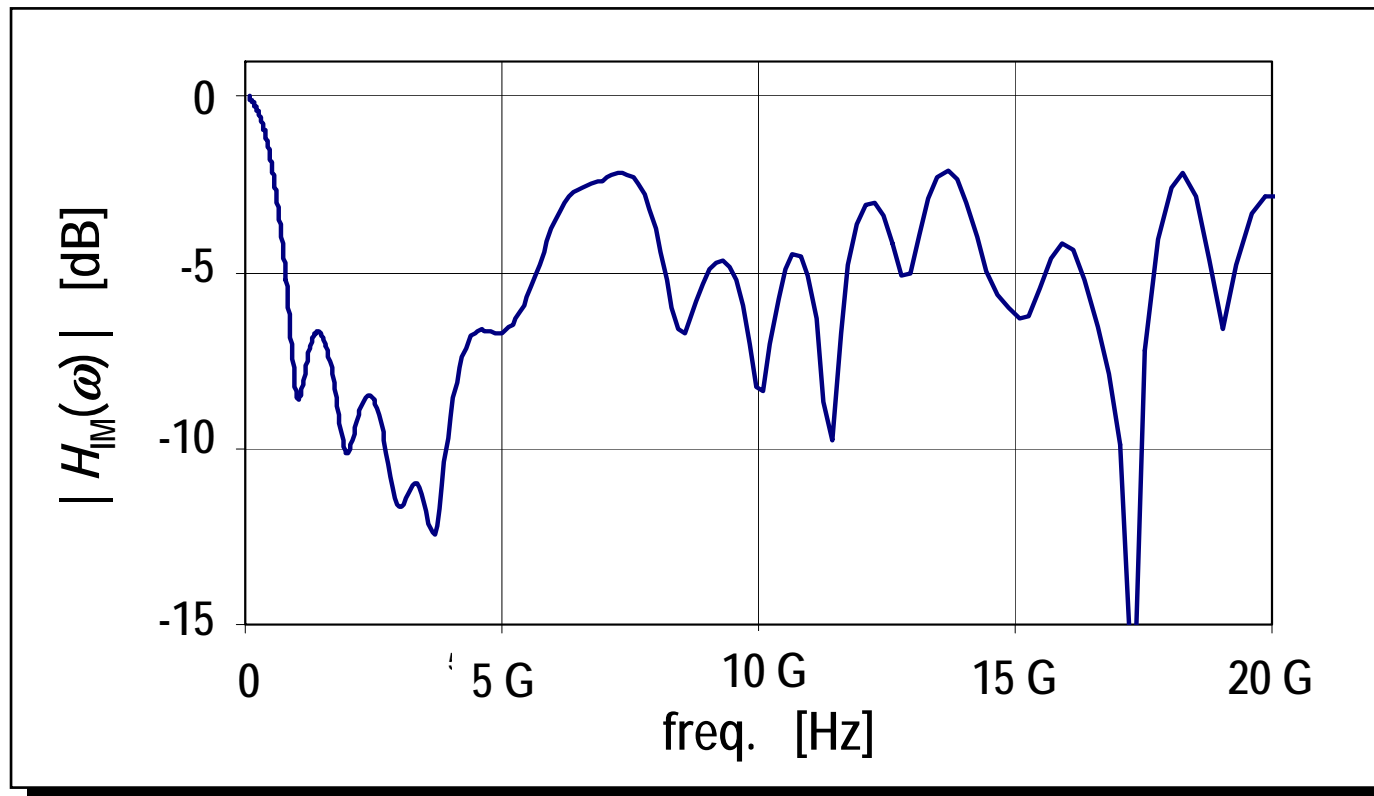


- MMF small signal intensity modulation transfer function due to modal dispersion, neglecting chromatic dispersion
 $|H_{MM}(\omega)| = \Phi_{out}(\omega) / \Phi_{in}(\omega)$
where $\Phi_{out}(\omega)$ is the Fourier transform of the output power signal $P_{out}(t)$ of the MMF, and $\Phi_{in}(\omega)$ of the input power signal $P_{in}(t)$
- neglecting chromatic dispersion, the impulse response of an MMF is a series of delayed impulses from the individual modes
→ frequency response $|H_{MM}(\omega)|$ shows multiple lobes
- without mode coupling: amplitudes of OFM generated harmonics can be shown to scale linearly with $|H_{MM}(\omega)|$
→ deploy the extended frequency response lobes of MMF
(or the wide frequency response of a well-equalised graded-index MMF)
- with mode coupling: the MMF itself also contributes to the OFM process;
→ the MZI contribution dominates as long as its delay τ exceeds the MMF's differential mode delays

[A.M.J. Koonen, A. Ng'oma, Wiley 2006]

[M. Garcia Larrode, A.M.J. Koonen, JLT 2008]

Higher-order transmission lobes in GI-MMF



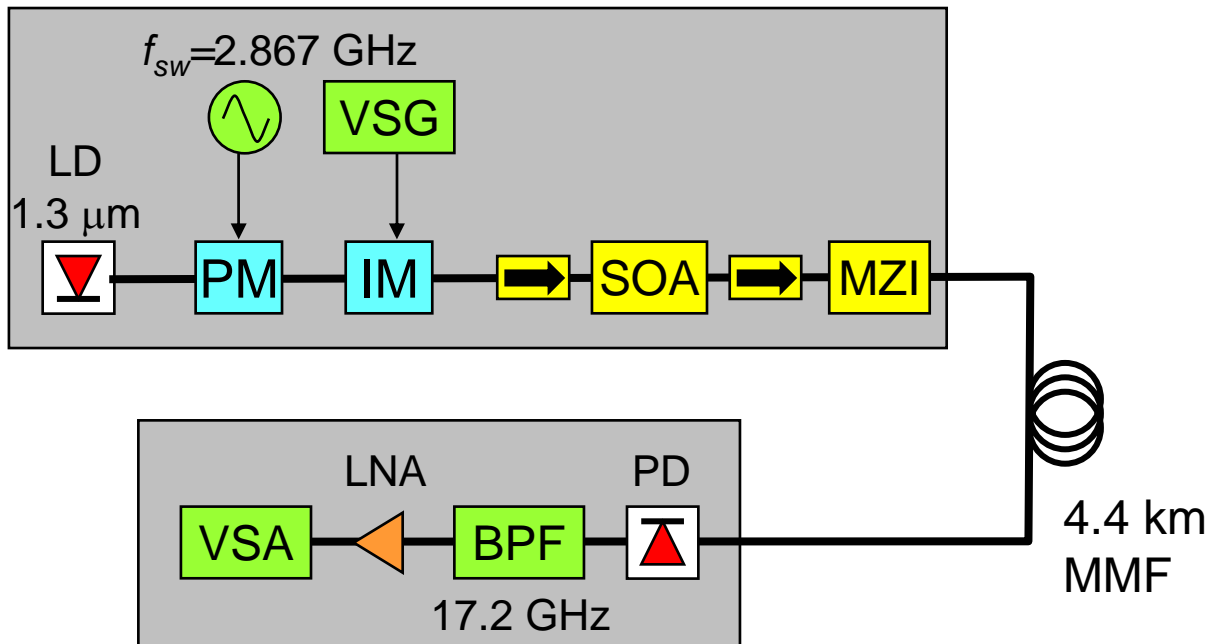
simulation

MMF length $L=5$ km
parabolic refr. index
core dia. $50 \mu\text{m}$

full NA launching, $NA=0.2$
negligible mode mixing

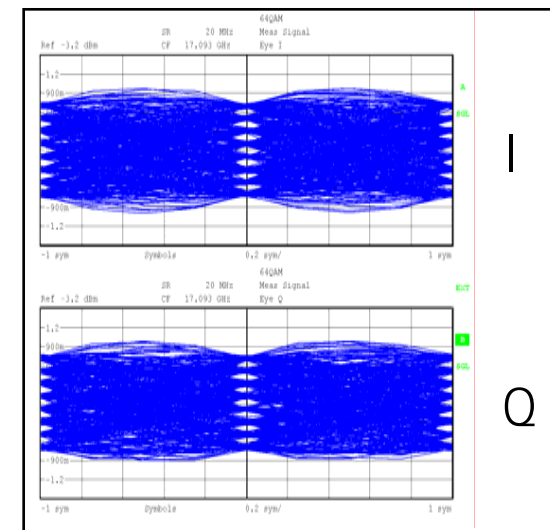
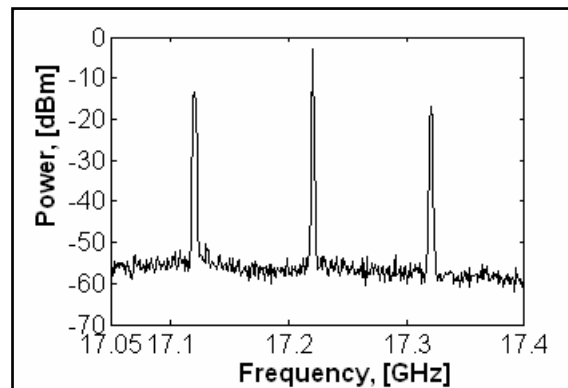
monochromatic source
 $\lambda=1.3 \mu\text{m}$

64-QAM experiment over silica GI-MMF



- μ -wave carrier freq. 17.2 GHz
- 64-QAM on subcarrier freq. 127 MHz
- symbol rate 20 MBaud \rightarrow 120 Mbit/s
- over 4.4 km silica GI-MMF
- also over 25 km SMF @ 39.9 GHz
- multi-tone (up to 10 tones) 64-QAM operation at 18.3 GHz over the GI-MMF link shown

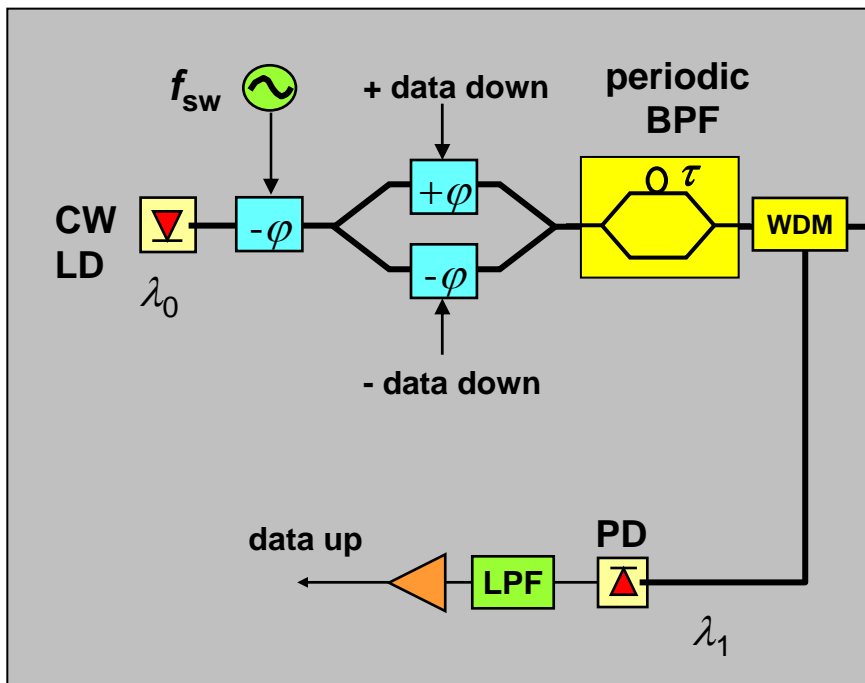
VSG = Vector Signal Generator
 VSA = Vector Signal Analyzer



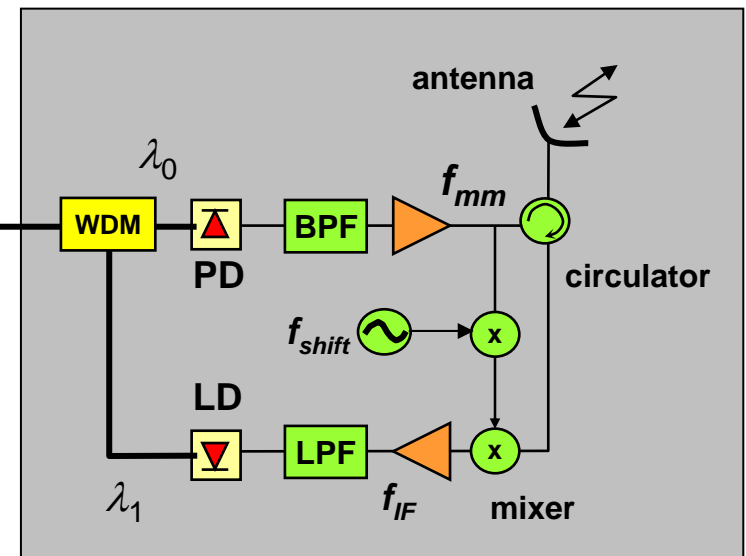
EVM = 4.8 % (< 5.6 % req.)

Bi-directional system

Central Station

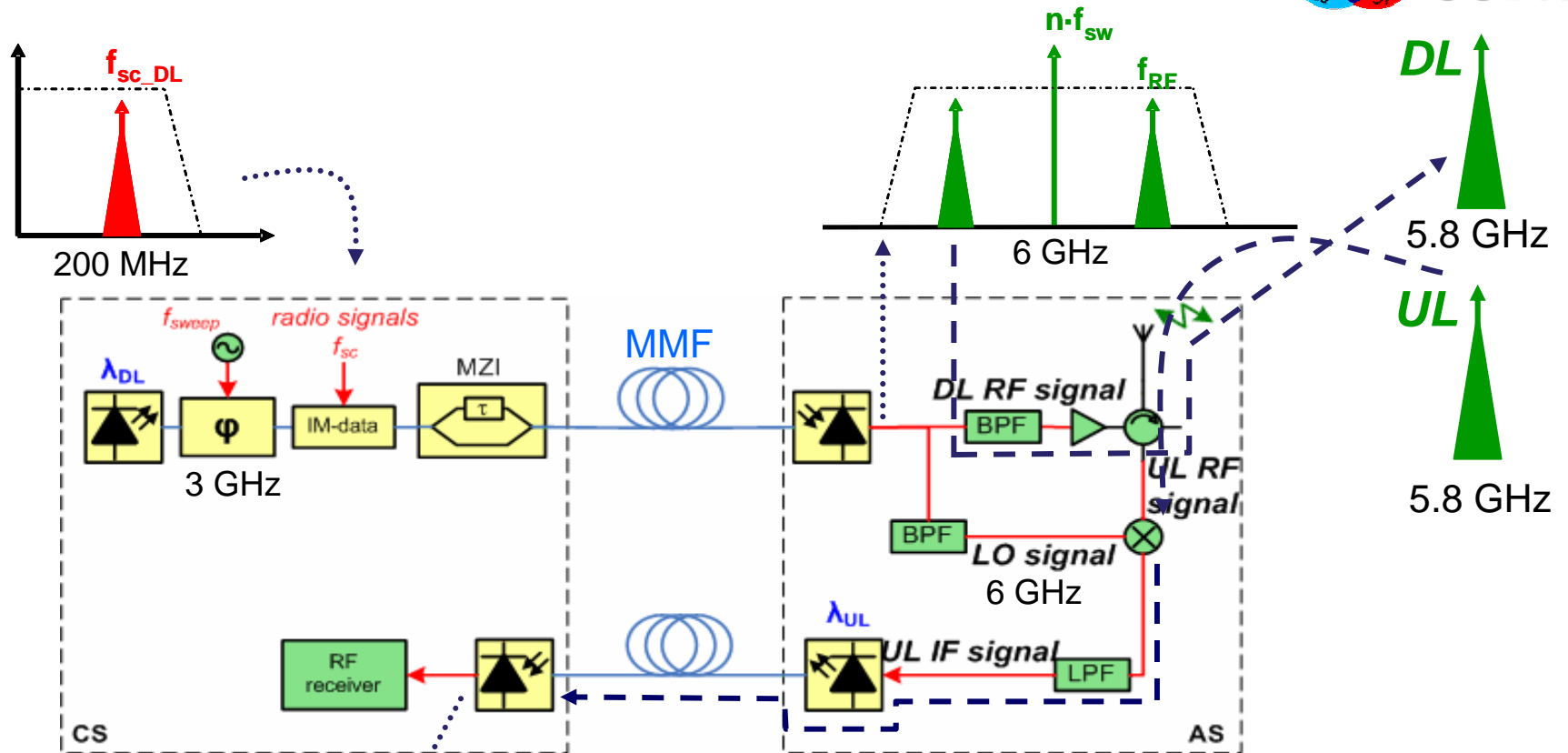


Antenna Station

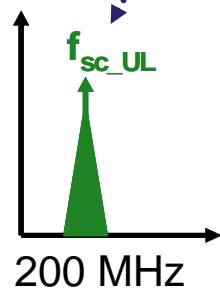


- freq.-division duplex
- upstream: TDMA, or SCMA, incl. MAC protocol

Bi-directional OFDM link



- Remote LO delivery
- Low cost uplink



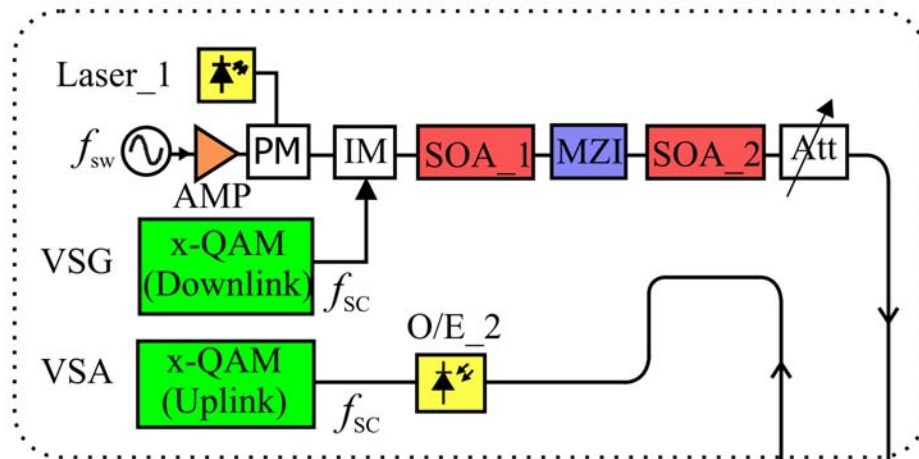
DL: 64-QAM, 24Mbit/s, at 5.8 GHz; $f_{sc_DL}=200\text{MHz}$
 $f_{LO}=6\text{ GHz}$
 4.4 km silica GI-MMF
 UL: 64-QAM, 24Mbit/s, at $f_{IF_UL}=200\text{MHz}$



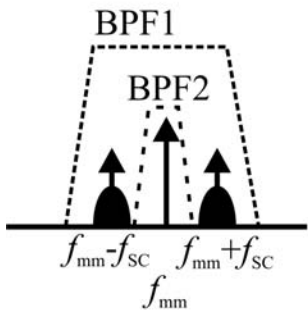
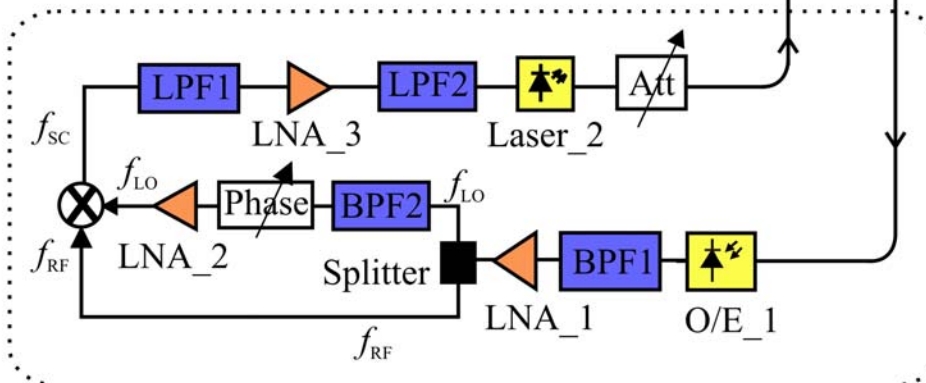
Bi-dir. 16-QAM experiment over GI-POF



Headend

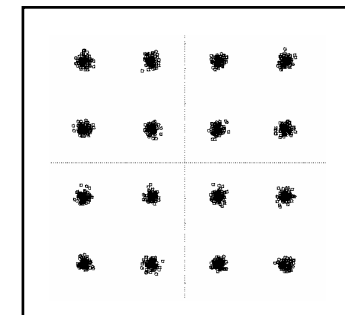


Remote Antenna Unit



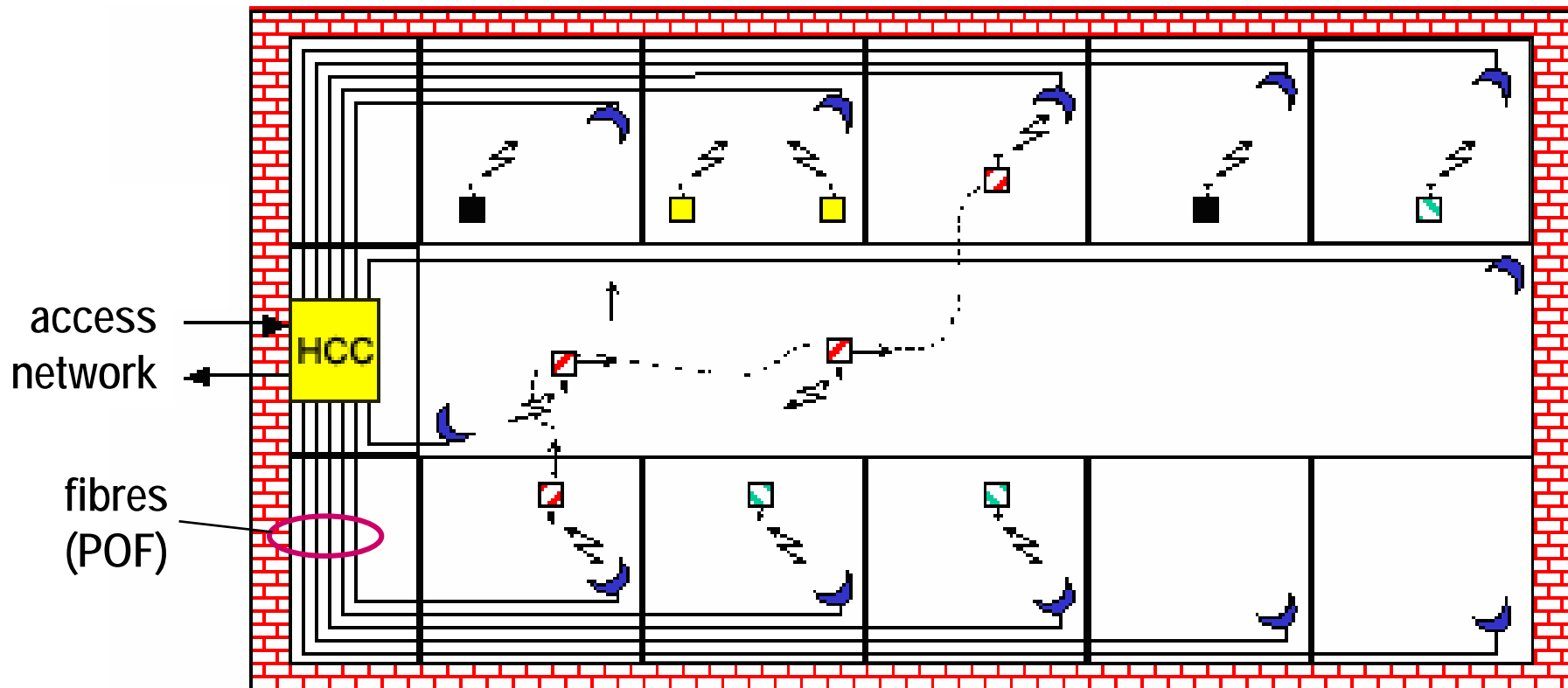
- downstream and upstream link: 100m 50 μ m core GI-POF
- PD BW=25 GHz, 50 μ m core MMF
- $\lambda_{\text{down}} = 1316 \text{ nm}$
- sweep freq. $f_{sw} = 2.867 \text{ GHz}$
- μ -wave carrier freq. 17.2 GHz (6th harmonic)
- subcarrier freq. 300 MHz
- symbol rate 25 MBaud \rightarrow 100 Mbit/s

POE
Fibres
(100m)



Constellation diagram
EVM=4.8% (<5.6%)

Inter-room μ -wave wireless communication

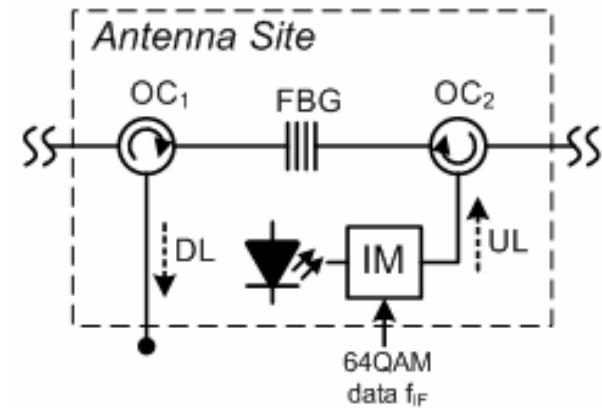
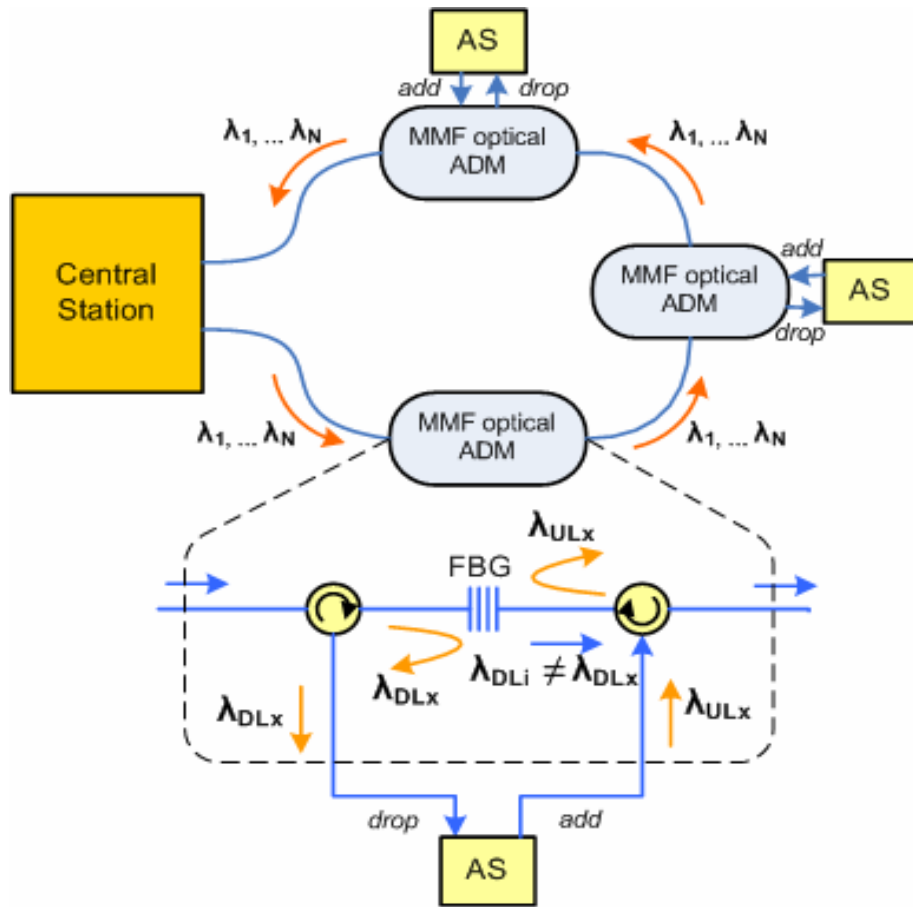


HCC: Home Communication Controller

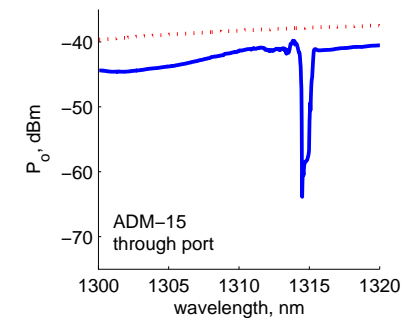
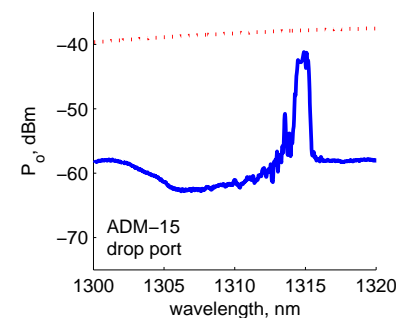
- transparent for any wireless signal format
- any-to-any room communication
- multi-casting



Wavelength-routed RoMMF network



- **RoMMF add/drop node**
(MMF FBG with BW=100 GHz)



- Downlink: 120 Mbit/s 64-QAM, at 23.7 GHz
- Uplink: 64-QAM, at $f_{IF}=300$ MHz, with IM/DD
- $\lambda_1=1303.8$ nm, $\lambda_2=1310.1$ nm, $\lambda_3=1314.8$ nm

- **drop and through ports**

Concluding remarks



- Future-proof, versatile and high-capacity service provisioning of multiple services in in-home networks can efficiently be done using *silica or polymer multimode fibre*.
- *Radio-over-fibre* facilitates the overlay of wireless communication services in a wired infrastructure, and the convergence of wirebound and wireless services in In-Home networks.
- With the *Optical Frequency Multiplying technique* microwave radio signals with high spectral purity and high capacity can be generated, and transported over dispersive multimode (and single-mode) fibre links.
- In combination with flexible wavelength routing, *reconfigurable multi-standard wireless pico-cell LANs* can be created.

Acknowledgement



Funding from

- the European Commission, in

FP7 project *ALPHA – Architectures for fLexible Photonic Home and Access networks*,

FP6 Network of Excellence *e-Photon/ONe* +,

FP6 Network of Excellence *ISIS*,

FP7 Network of Excellence *BONE*

- the Dutch Ministry of Economic Affairs, in the IOP Generieke Communicatie projects *RoF Broadband In-House Systems* and *Future Home Networks*

is gratefully acknowledged.

